

## MEMORANDUM

**Date:** March 3, 2025

**To:** Town of Rolesville, NC

**From:** Timothy G. Nifong, PE

**Subject:** Public and Private Storm Sewer Pipe Network Design – Hall of Fame Car Wash – Rolesville, Wake County, NC



### Project Summary

The purpose of this memorandum is to present the design calculations for the public and private storm sewer pipe network for the Hall of Fame Car Wash site located on Lot 8 of the Wallbrook Development. The total development consists of approximately 7.04 acres. The site is located on the South side of Main Street (US 401) and East side of Wall Creek Drive in Rolesville, NC. (Reference Wallbrook Preliminary Plat PR21-04 REV, Wallbrook Lot 8 Preliminary Plat PSP24-06, and Hall of Fame Car Wash – Lot 8 SDP25-01).

Line 11 (504-DI) represents the future drainage from lot 8B as shown on PSP 24-06, totaling 1.67 acres to the proposed storm sewer system. Line 15 to 12 represents the outfall from the proposed underground stormwater detention system with a known flow (cfs) entered into Line 15.

### Calculation Methodology & Constants

- A minimum time of concentration of 5 minutes was utilized
- A minimum rational C value of 0.60 was utilized for open space areas
- A minimum rational C value of 0.95 was utilized for built-upon areas
- All pipes are RCP using a Manning's n value of 0.013
- The minimum pipe size used is 15"
- Rainfall data was taken from NOAA Atlas 14 at the Neuse 2 NE station

### Analysis

The pipe networks were modeled using Autodesk Civil 3D and the model data was exported to Hydraflow Storm Sewer software for analysis. The attached results show that the drainage network meets Wake County and Town of Rolesville regulations and standards as follows:

- The gutter spread for the 1-year, approximately 4 in/hr storm, does not encroach more than 10' into the adjacent driving lane for the public storm sewer system (101-CB, 102-CB, 502-CB, & 503-CB).
- The total flow (cfs) within the storm sewer system does not exceed the flow capacity (cfs) in the pipe network in the 10-year rain event for storm sewer system.
- The 10-yr rain event HGL is contained within the storm sewer system.

## **Drainage Area Map and Supporting Documents**



**NOAA Atlas 14, Volume 2, Version 3**  
**Location name: Raleigh, North Carolina, USA\***  
**Latitude: 35.9167°, Longitude: -78.5667°**  
**Elevation: 243.35 ft\*\***

\* source: ESRI Maps

\*\* source: USGS



## POINT PRECIPITATION FREQUENCY ESTIMATES

G.M. Bonnin, D. Martin, B. Lin, T. Parzybok, M. Yekta, and D. Riley

NOAA, National Weather Service, Silver Spring, Maryland

[PF tabular](#) | [PF graphical](#) | [Maps & aerials](#)

### PF tabular

Duration	Average recurrence interval (years)									
	1	2	5	10	25	50	100	200	500	1000
5-min	<b>4.82</b> (4.42-5.28)	<b>5.62</b> (5.15-6.13)	<b>6.42</b> (5.89-7.01)	<b>7.18</b> (6.56-7.82)	<b>7.94</b> (7.24-8.66)	<b>8.53</b> (7.74-9.30)	<b>9.06</b> (8.16-9.86)	<b>9.50</b> (8.53-10.4)	<b>10.0</b> (8.90-10.9)	<b>10.4</b> (9.20-11.4)
10-min	<b>3.85</b> (3.53-4.21)	<b>4.49</b> (4.12-4.91)	<b>5.15</b> (4.72-5.62)	<b>5.74</b> (5.25-6.26)	<b>6.33</b> (5.77-6.90)	<b>6.79</b> (6.16-7.40)	<b>7.19</b> (6.49-7.84)	<b>7.54</b> (6.76-8.23)	<b>7.92</b> (7.04-8.64)	<b>8.22</b> (7.25-8.99)
15-min	<b>3.21</b> (2.94-3.51)	<b>3.76</b> (3.45-4.11)	<b>4.34</b> (3.98-4.74)	<b>4.84</b> (4.43-5.28)	<b>5.35</b> (4.87-5.83)	<b>5.74</b> (5.20-6.25)	<b>6.06</b> (5.47-6.60)	<b>6.34</b> (5.68-6.92)	<b>6.64</b> (5.91-7.25)	<b>6.88</b> (6.06-7.52)
30-min	<b>2.20</b> (2.02-2.41)	<b>2.60</b> (2.38-2.84)	<b>3.08</b> (2.83-3.36)	<b>3.51</b> (3.21-3.82)	<b>3.96</b> (3.61-4.32)	<b>4.32</b> (3.92-4.71)	<b>4.64</b> (4.19-5.06)	<b>4.93</b> (4.42-5.38)	<b>5.29</b> (4.70-5.77)	<b>5.57</b> (4.91-6.09)
60-min	<b>1.37</b> (1.26-1.50)	<b>1.63</b> (1.50-1.78)	<b>1.98</b> (1.81-2.16)	<b>2.28</b> (2.09-2.49)	<b>2.64</b> (2.40-2.88)	<b>2.93</b> (2.65-3.19)	<b>3.20</b> (2.88-3.48)	<b>3.46</b> (3.10-3.78)	<b>3.79</b> (3.37-4.14)	<b>4.07</b> (3.59-4.44)
2-hr	<b>0.800</b> (0.728-0.883)	<b>0.956</b> (0.872-1.05)	<b>1.17</b> (1.06-1.28)	<b>1.36</b> (1.24-1.50)	<b>1.60</b> (1.44-1.75)	<b>1.80</b> (1.61-1.97)	<b>1.99</b> (1.77-2.17)	<b>2.18</b> (1.93-2.38)	<b>2.43</b> (2.13-2.65)	<b>2.64</b> (2.30-2.89)
3-hr	<b>0.565</b> (0.514-0.625)	<b>0.675</b> (0.616-0.744)	<b>0.829</b> (0.755-0.913)	<b>0.974</b> (0.884-1.07)	<b>1.15</b> (1.04-1.26)	<b>1.31</b> (1.17-1.43)	<b>1.46</b> (1.30-1.60)	<b>1.62</b> (1.43-1.77)	<b>1.83</b> (1.60-2.00)	<b>2.01</b> (1.74-2.21)
6-hr	<b>0.340</b> (0.311-0.375)	<b>0.407</b> (0.373-0.447)	<b>0.500</b> (0.457-0.549)	<b>0.588</b> (0.536-0.644)	<b>0.699</b> (0.632-0.764)	<b>0.796</b> (0.716-0.869)	<b>0.893</b> (0.796-0.973)	<b>0.994</b> (0.877-1.08)	<b>1.13</b> (0.985-1.23)	<b>1.25</b> (1.08-1.37)
12-hr	<b>0.200</b> (0.183-0.220)	<b>0.239</b> (0.220-0.261)	<b>0.295</b> (0.270-0.323)	<b>0.349</b> (0.318-0.381)	<b>0.417</b> (0.378-0.455)	<b>0.478</b> (0.431-0.519)	<b>0.540</b> (0.481-0.586)	<b>0.606</b> (0.534-0.657)	<b>0.697</b> (0.604-0.754)	<b>0.778</b> (0.664-0.843)
24-hr	<b>0.119</b> (0.111-0.128)	<b>0.144</b> (0.134-0.154)	<b>0.180</b> (0.168-0.193)	<b>0.209</b> (0.194-0.224)	<b>0.248</b> (0.230-0.266)	<b>0.279</b> (0.258-0.299)	<b>0.310</b> (0.286-0.333)	<b>0.343</b> (0.315-0.368)	<b>0.387</b> (0.355-0.415)	<b>0.422</b> (0.385-0.454)
2-day	<b>0.069</b> (0.064-0.074)	<b>0.083</b> (0.078-0.089)	<b>0.103</b> (0.096-0.111)	<b>0.119</b> (0.111-0.128)	<b>0.141</b> (0.131-0.151)	<b>0.158</b> (0.146-0.169)	<b>0.175</b> (0.162-0.188)	<b>0.192</b> (0.177-0.207)	<b>0.217</b> (0.199-0.233)	<b>0.235</b> (0.215-0.254)
3-day	<b>0.049</b> (0.046-0.052)	<b>0.059</b> (0.055-0.063)	<b>0.073</b> (0.068-0.078)	<b>0.083</b> (0.078-0.089)	<b>0.098</b> (0.092-0.105)	<b>0.110</b> (0.102-0.118)	<b>0.122</b> (0.113-0.131)	<b>0.134</b> (0.124-0.144)	<b>0.151</b> (0.139-0.162)	<b>0.165</b> (0.150-0.177)
4-day	<b>0.039</b> (0.036-0.041)	<b>0.046</b> (0.043-0.049)	<b>0.057</b> (0.054-0.061)	<b>0.066</b> (0.061-0.070)	<b>0.077</b> (0.072-0.082)	<b>0.086</b> (0.080-0.092)	<b>0.096</b> (0.089-0.102)	<b>0.105</b> (0.097-0.113)	<b>0.119</b> (0.109-0.127)	<b>0.129</b> (0.118-0.138)
7-day	<b>0.026</b> (0.024-0.027)	<b>0.031</b> (0.029-0.032)	<b>0.037</b> (0.035-0.040)	<b>0.042</b> (0.040-0.045)	<b>0.050</b> (0.046-0.053)	<b>0.055</b> (0.052-0.059)	<b>0.061</b> (0.052-0.065)	<b>0.067</b> (0.057-0.065)	<b>0.075</b> (0.062-0.072)	<b>0.082</b> (0.069-0.080)
10-day	<b>0.020</b> (0.019-0.022)	<b>0.024</b> (0.023-0.026)	<b>0.029</b> (0.027-0.031)	<b>0.033</b> (0.031-0.035)	<b>0.038</b> (0.036-0.041)	<b>0.042</b> (0.039-0.045)	<b>0.046</b> (0.043-0.049)	<b>0.050</b> (0.047-0.054)	<b>0.056</b> (0.052-0.060)	<b>0.060</b> (0.056-0.065)
20-day	<b>0.014</b> (0.013-0.015)	<b>0.016</b> (0.015-0.017)	<b>0.019</b> (0.018-0.020)	<b>0.021</b> (0.020-0.023)	<b>0.024</b> (0.023-0.026)	<b>0.027</b> (0.025-0.029)	<b>0.029</b> (0.027-0.031)	<b>0.032</b> (0.030-0.034)	<b>0.035</b> (0.033-0.038)	<b>0.038</b> (0.035-0.041)
30-day	<b>0.011</b> (0.011-0.012)	<b>0.013</b> (0.013-0.014)	<b>0.015</b> (0.015-0.016)	<b>0.017</b> (0.016-0.018)	<b>0.019</b> (0.018-0.021)	<b>0.021</b> (0.020-0.022)	<b>0.023</b> (0.021-0.024)	<b>0.024</b> (0.023-0.026)	<b>0.027</b> (0.025-0.028)	<b>0.028</b> (0.026-0.030)
45-day	<b>0.010</b> (0.009-0.010)	<b>0.011</b> (0.011-0.012)	<b>0.013</b> (0.012-0.014)	<b>0.014</b> (0.013-0.015)	<b>0.016</b> (0.015-0.017)	<b>0.017</b> (0.016-0.018)	<b>0.018</b> (0.017-0.019)	<b>0.019</b> (0.018-0.020)	<b>0.021</b> (0.020-0.022)	<b>0.022</b> (0.021-0.023)
60-day	<b>0.009</b> (0.008-0.009)	<b>0.010</b> (0.010-0.011)	<b>0.011</b> (0.011-0.012)	<b>0.012</b> (0.012-0.013)	<b>0.014</b> (0.013-0.014)	<b>0.015</b> (0.014-0.015)	<b>0.016</b> (0.015-0.016)	<b>0.017</b> (0.016-0.017)	<b>0.018</b> (0.017-0.019)	<b>0.019</b> (0.018-0.020)

<sup>1</sup> Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS).

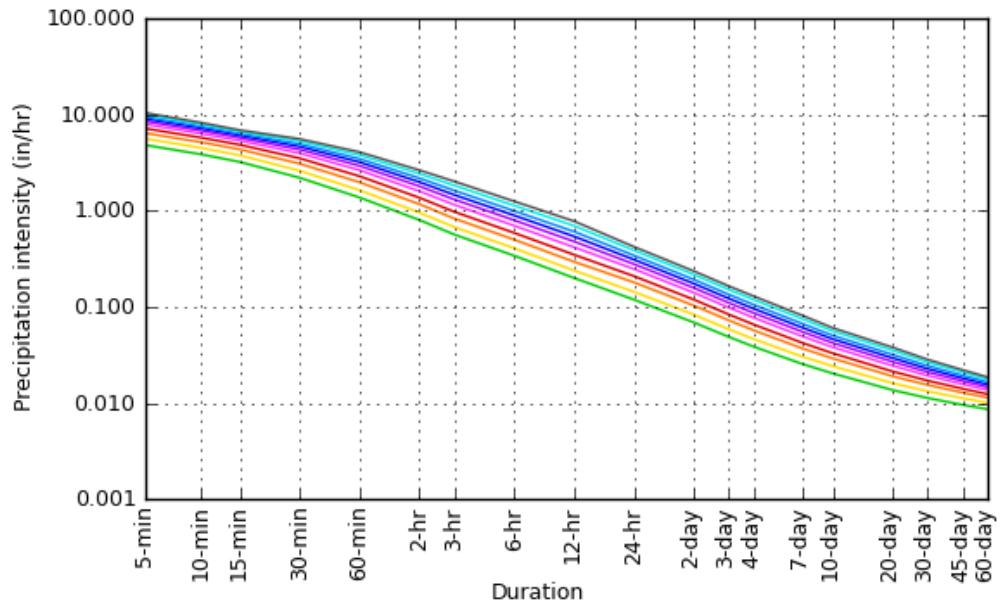
Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values.

Please refer to NOAA Atlas 14 document for more information.

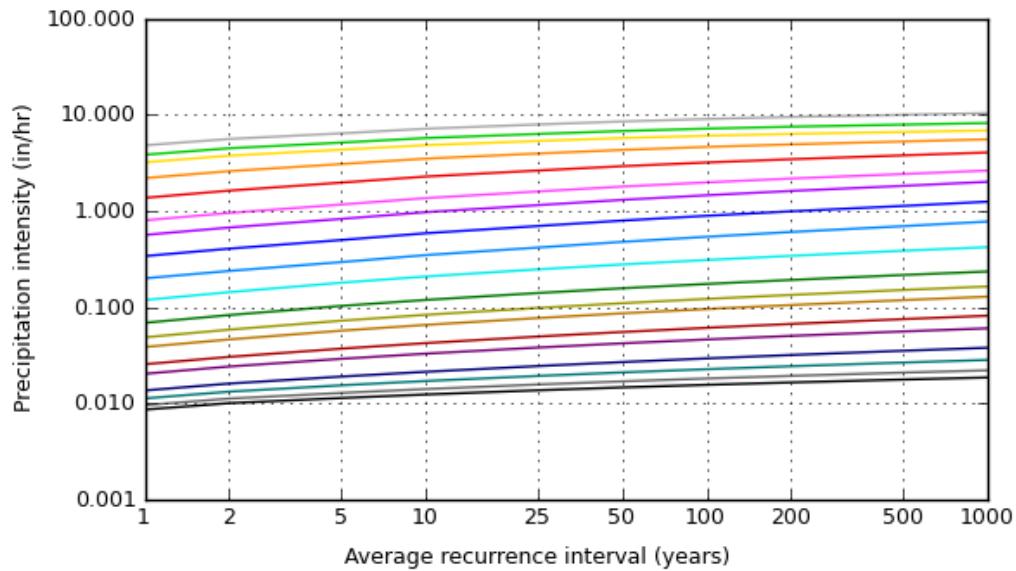
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### PF graphical

PDS-based intensity-duration-frequency (IDF) curves  
Latitude: 35.9167°, Longitude: -78.5667°



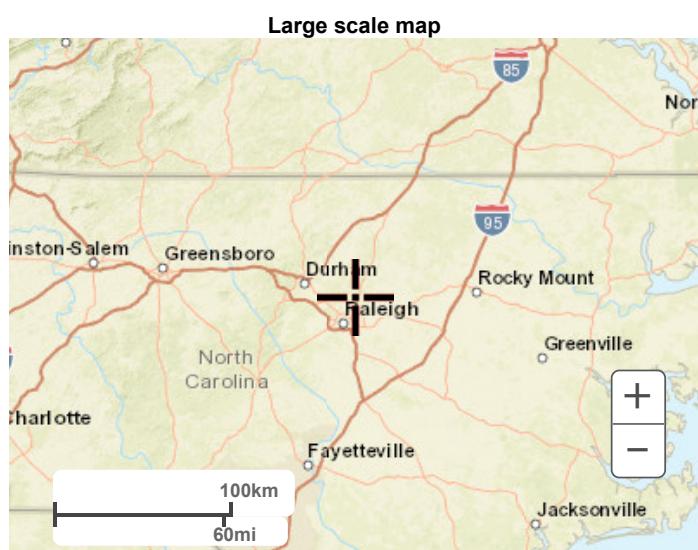
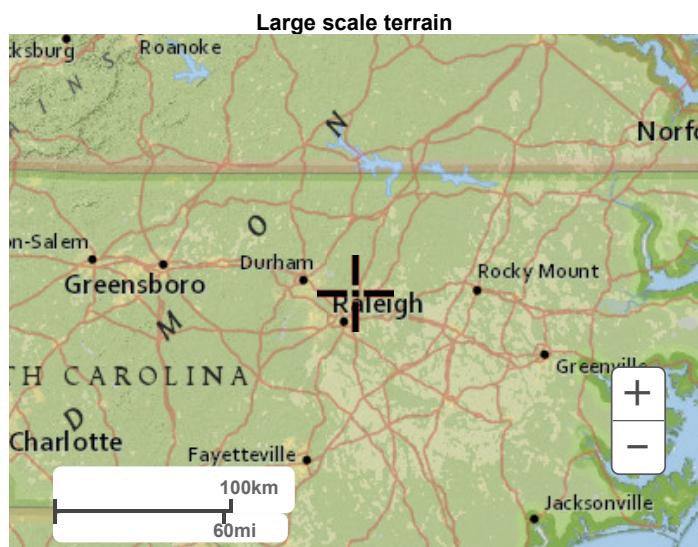
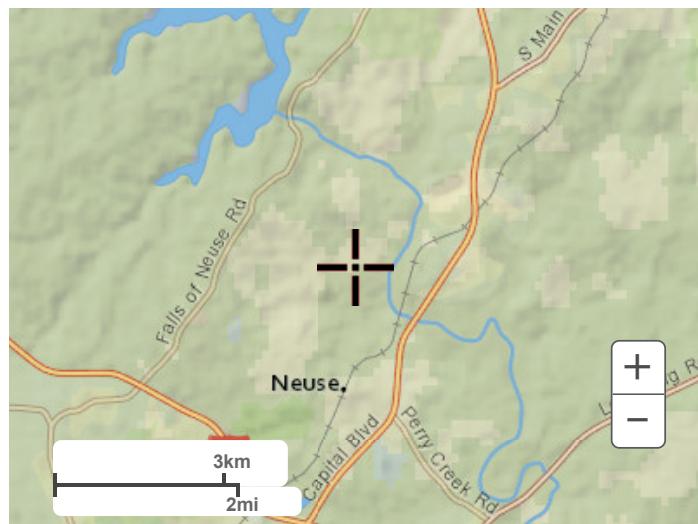
Average recurrence interval (years)
1
2
5
10
25
50
100
200
500
1000



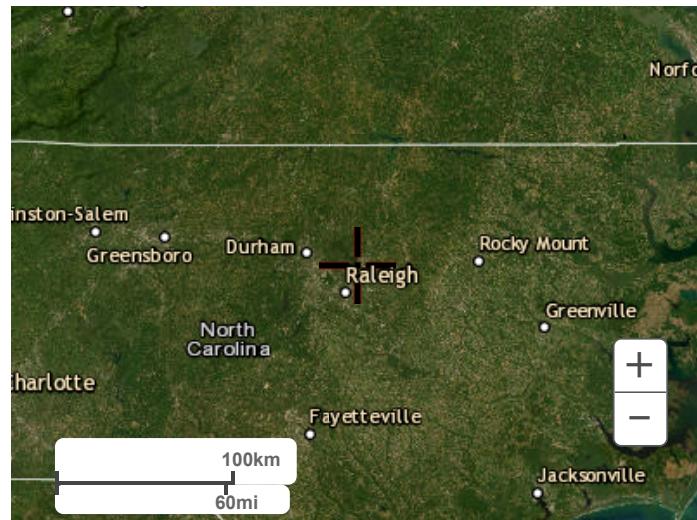
Duration	
5-min	2-day
10-min	3-day
15-min	4-day
30-min	7-day
60-min	10-day
2-hr	20-day
3-hr	30-day
6-hr	45-day
12-hr	60-day
24-hr	

## Maps & aerials

[Small scale terrain](#)



Large scale aerial



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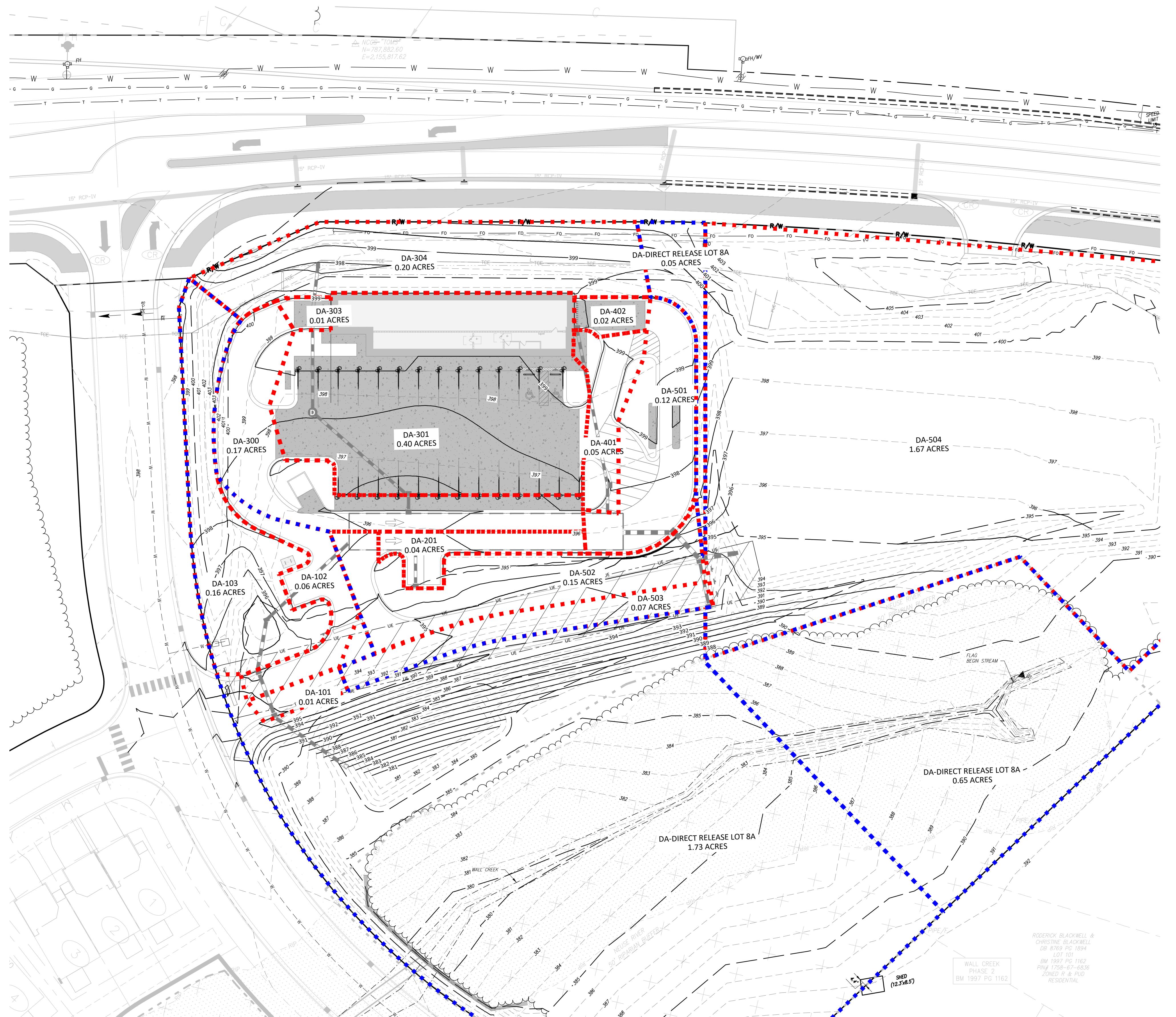
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[US Department of Commerce](#)  
[National Oceanic and Atmospheric Administration](#)  
[National Weather Service](#)  
[National Water Center](#)  
1325 East West Highway  
Silver Spring, MD 20910  
Questions?: [HDSC.Questions@noaa.gov](mailto:HDSC.Questions@noaa.gov)

[Disclaimer](#)

REVISIONS:	
2 3-MAR-25	REVISED PER TRC REVIEW COMMENTS
2 2-MAR-25	INITIAL SUBMITTAL FOR REVIEW
# DATE	DESCRIPTION

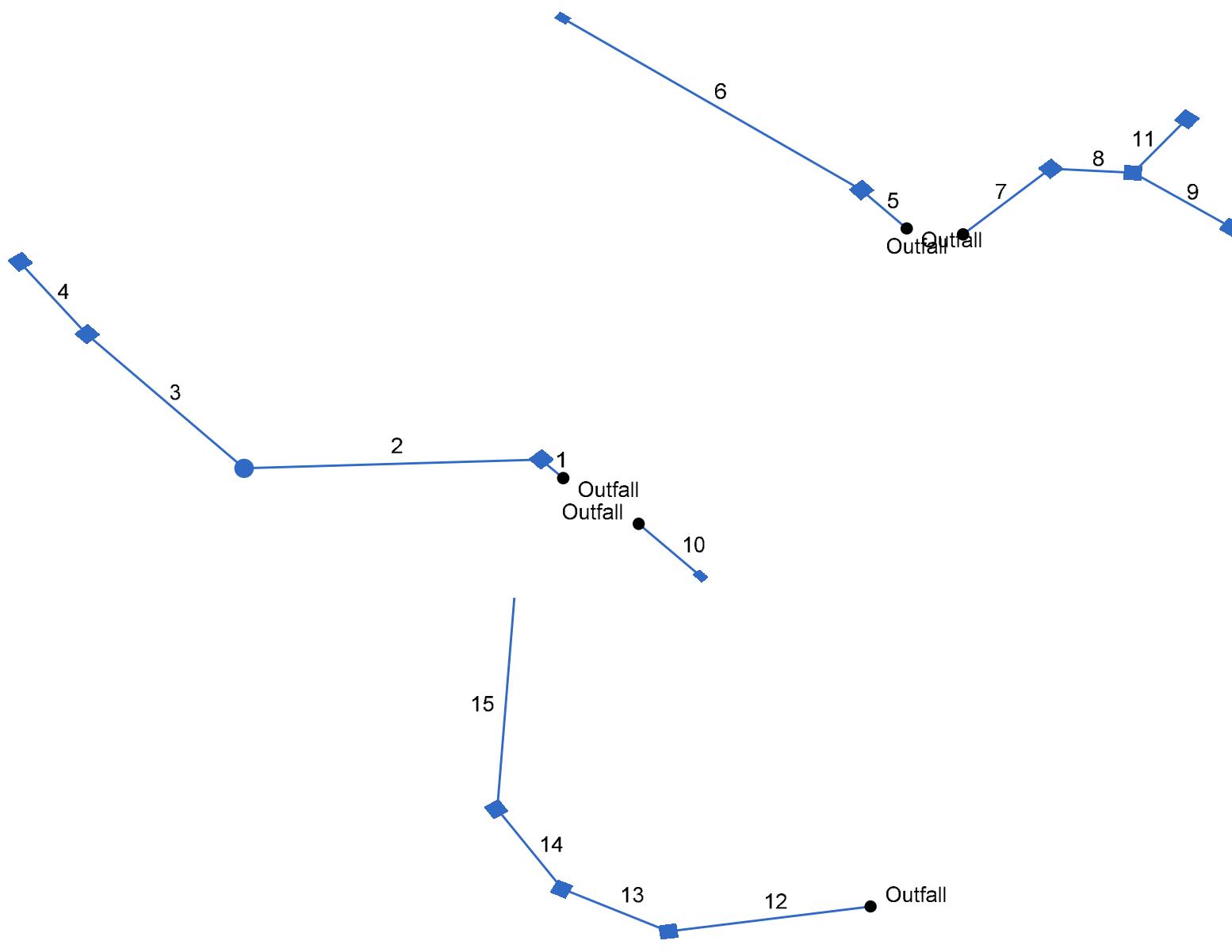
**DRAINAGE AREA MAP**  
**HALL OF FAME CAR WASH**  
**WALLBROOK - LOT 8**  
**Town of Rolesville Project No. SDP 25-01**  
**US 401 Business / S. Main Street & Wall Creek Drive**  
**Wake Forest Township, Town of Rolesville, North Carolina**



30'  
0  
15'  
30'  
SCALE 1 inch = 30 ft

Date: January 2, 2025

# Hydraflow Storm Sewers Extension for Autodesk® Civil 3D® Plan



## **1-Year Rain Event Results for Gutter Spread**

## Inlets

Line No.	Inlet ID	Drng Area	Inlet Time	i Inlet	Runoff Coeff	Flow Rate	Line Type	Grate Area	Cross Sl, Sw	Cross Sl, Sx	Local Depr	Gutter Spread	Gutter Depth	
		(ac)	(min)	(in/hr)	(C)	(cfs)		(sqft)	(ft/ft)	(ft/ft)	(in)	(ft)	(ft)	
15	104-UGO	0.00	0.0	0.00	0.00	4.67	Cir	....	....	....	....	....	....	
14	103-DI	0.16	5.0	4.82	0.60	5.13	Cir	3.10	0.056	0.020	2.0	1.13	-0.01	
13	102-CB	0.06	5.0	4.82	0.95	5.40	Cir	....	0.056	0.020	2.0	2.44	0.12	
12	101-CB	0.01	5.0	4.82	0.95	5.44	Cir	....	0.056	0.020	2.0	1.10	0.06	
11	504-DI	1.67	5.0	4.82	0.90	7.24	Cir	3.10	0.056	0.020	2.0	19.61	0.46	
10	201-CB	0.04	5.0	4.82	0.95	0.18	Cir	3.10	0.056	0.020	2.0	0.90	-0.04	
9	503-CB	0.07	5.0	4.82	0.95	0.32	Cir	3.10	0.056	0.020	2.0	1.23	0.01	
8	502-CB	0.15	5.0	4.82	0.95	7.57	Cir	3.10	0.056	0.020	2.0	1.87	0.09	
7	501-CB	0.12	5.0	4.82	0.95	8.03	Cir	3.10	0.056	0.020	2.0	1.66	0.06	
6	402-CB	0.02	5.0	4.82	0.95	0.09	Cir	3.10	0.056	0.020	2.0	0.60	-0.08	
5	401-CB	0.05	5.0	4.82	0.95	0.17	Cir	3.10	0.056	0.020	2.0	1.02	-0.02	
4	304-DI	0.20	5.0	4.82	0.60	0.58	Cir	3.10	0.056	0.020	2.0	1.31	0.02	
3	303-DI	0.01	5.0	4.82	0.95	0.60	Cir	3.10	0.056	0.020	2.0	0.24	-0.13	
2	302-JB	0.00	5.0	0.00	0.00	0.55	Cir	....	....	....	....	....	....	
1	301-CB	0.40	5.0	4.82	0.95	1.96	Cir	3.10	0.056	0.020	2.0	4.03	0.15	

Project File: 2025-03-03 - Lot 8A HoF.stm

Number of lines: 15

Date: 3/3/2025

NOTES: Intensity =  $62.18 / (\text{Inlet time} + 12.70)^{0.89}$  -- Return period = 1 Yrs. ; \*\* Critical depth

## **10-Year Rain Event Results**

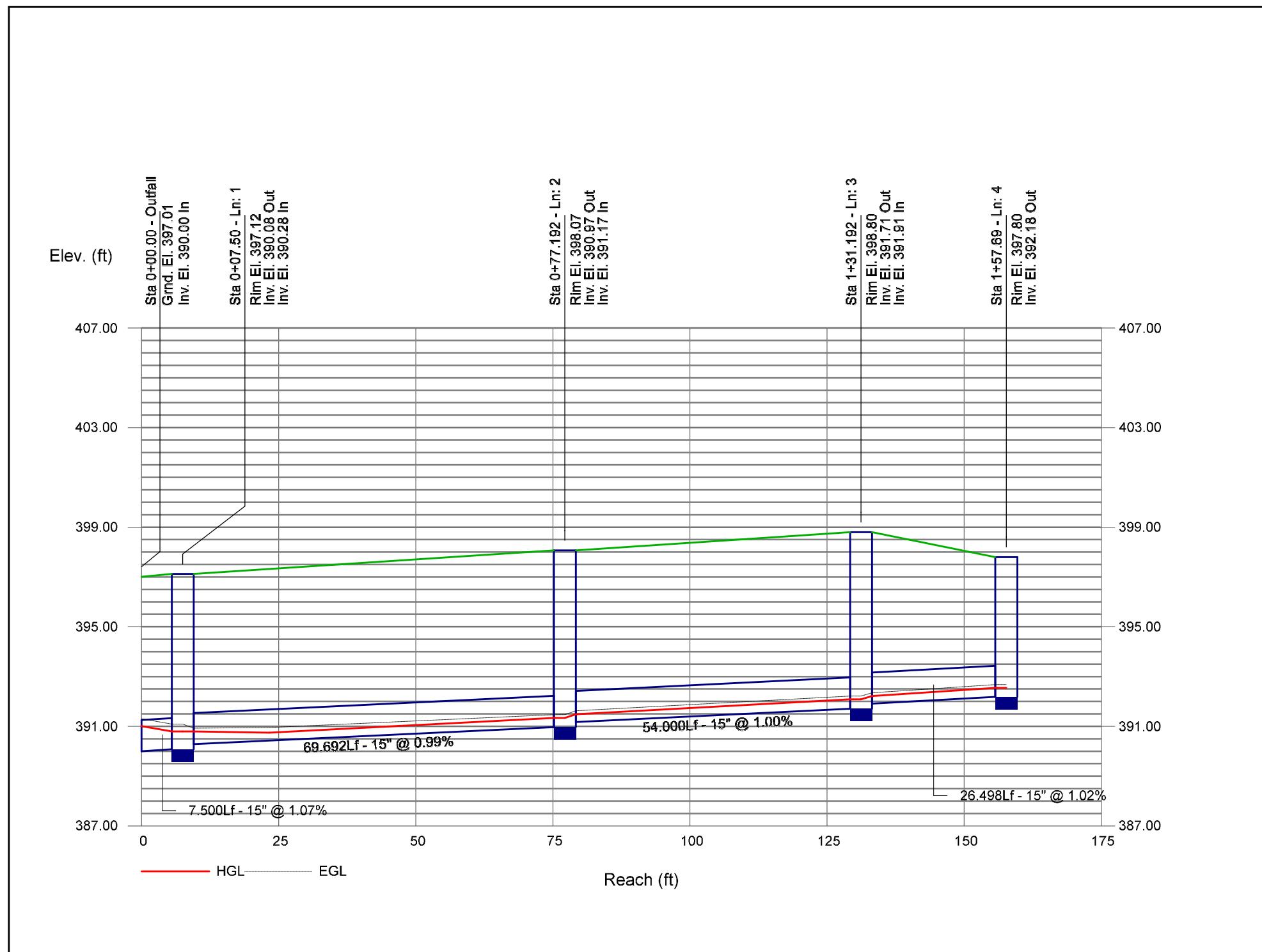
# Storm Sewer Tabulation

Station		Len	Drng Area		Rnoff coeff	Area x C		Tc		Rain (I)	Total flow	Cap full	Vel	Pipe		Invert Elev		HGL Elev		Grnd / Rim Elev		Line ID
Line	To Line		Incr (ft)	Total (ac)		Incr	Total	Inlet (min)	Syst (min)					Size (in)	Slope (%)	Dn (ft)	Up (ft)	Dn (ft)	Up (ft)	Dn (ft)	Up (ft)	
1	End	7.500	0.40	0.61	0.95	0.38	0.51	5.0	8.4	6.2	3.17	6.67	3.67	15	1.07	390.00	390.08	391.01	390.80	397.01	397.12	301
2	1	69.692	0.00	0.21	0.00	0.00	0.13	5.0	6.8	6.6	0.86	6.43	2.35	15	0.99	390.28	390.97	390.80	391.33	397.12	398.07	302
3	2	54.000	0.01	0.21	0.95	0.01	0.13	5.0	5.6	7.0	0.90	6.46	3.33	15	1.00	391.17	391.71	391.49	392.08	398.07	398.80	303
4	3	26.498	0.20	0.20	0.60	0.12	0.12	5.0	5.0	7.2	0.86	6.52	3.29	15	1.02	391.91	392.18	392.22	392.54	398.80	397.80	304
5	End	15.500	0.05	0.07	0.95	0.05	0.07	5.0	18.0	4.6	0.31	9.13	1.27	15	2.00	390.00	390.31	390.82	390.52	391.80	398.45	401
6	5	86.450	0.02	0.02	0.95	0.02	0.02	5.0	5.0	7.2	0.14	9.13	2.23	15	2.00	390.51	392.24	390.62	392.38	398.45	399.47	402
7	End	28.107	0.12	2.01	0.95	0.11	1.83	5.0	6.3	6.8	12.38	15.96	5.03	24	0.50	388.50	388.64	390.00	390.07	390.88	397.62	501
8	7	19.578	0.15	1.89	0.95	0.14	1.71	5.0	6.2	6.8	11.65	16.17	4.16	24	0.51	388.84	388.94	390.54	390.57	397.62	393.84	502
9	8	28.000	0.07	0.07	0.95	0.07	0.07	5.0	5.0	7.2	0.48	4.57	0.75	15	0.50	390.21	390.35	390.93	390.93	393.84	393.84	503
10	End	21.000	0.04	0.04	0.95	0.04	0.04	5.0	5.0	7.2	0.27	9.13	1.25	15	2.00	389.58	390.00	390.29	390.20	391.10	396.58	201
11	8	20.039	1.67	1.67	0.90	1.50	1.50	5.0	5.0	7.2	10.79	15.98	3.70	24	0.50	389.14	389.24	390.93	390.96	393.84	394.22	504
12	End	47.891	0.01	0.23	0.95	0.01	0.16	5.0	5.3	7.1	5.82	5.68	3.81	18	0.29	384.00	384.14	385.20	385.36	385.79	395.34	101
13	12	28.000	0.06	0.22	0.95	0.06	0.15	5.0	5.2	7.1	5.76	5.95	3.73	18	0.32	384.34	384.43	385.57	385.65	395.34	395.34	102
14	13	27.851	0.16	0.16	0.60	0.10	0.10	5.0	5.0	7.2	5.36	14.85	6.31	18	2.00	386.31	386.86	386.93	387.76	395.34	394.20	103
15	14	61.800	0.00	0.00	0.00	0.00	0.00	0.0	0.0	0.0	4.67	9.15	5.87	15	2.01	387.06	388.30	387.76	389.18	394.20	390.10	105
Project File: 2025-03-03 - Lot 8A HoF.stm														Number of lines: 15				Run Date: 3/3/2025				
NOTES:Intensity = 73.11 / (Inlet time + 12.60) ^ 0.81; Return period =Yrs. 10 ; c = cir e = ellip b = box																						

## **10-Year Hydraulic Grade Profiles**

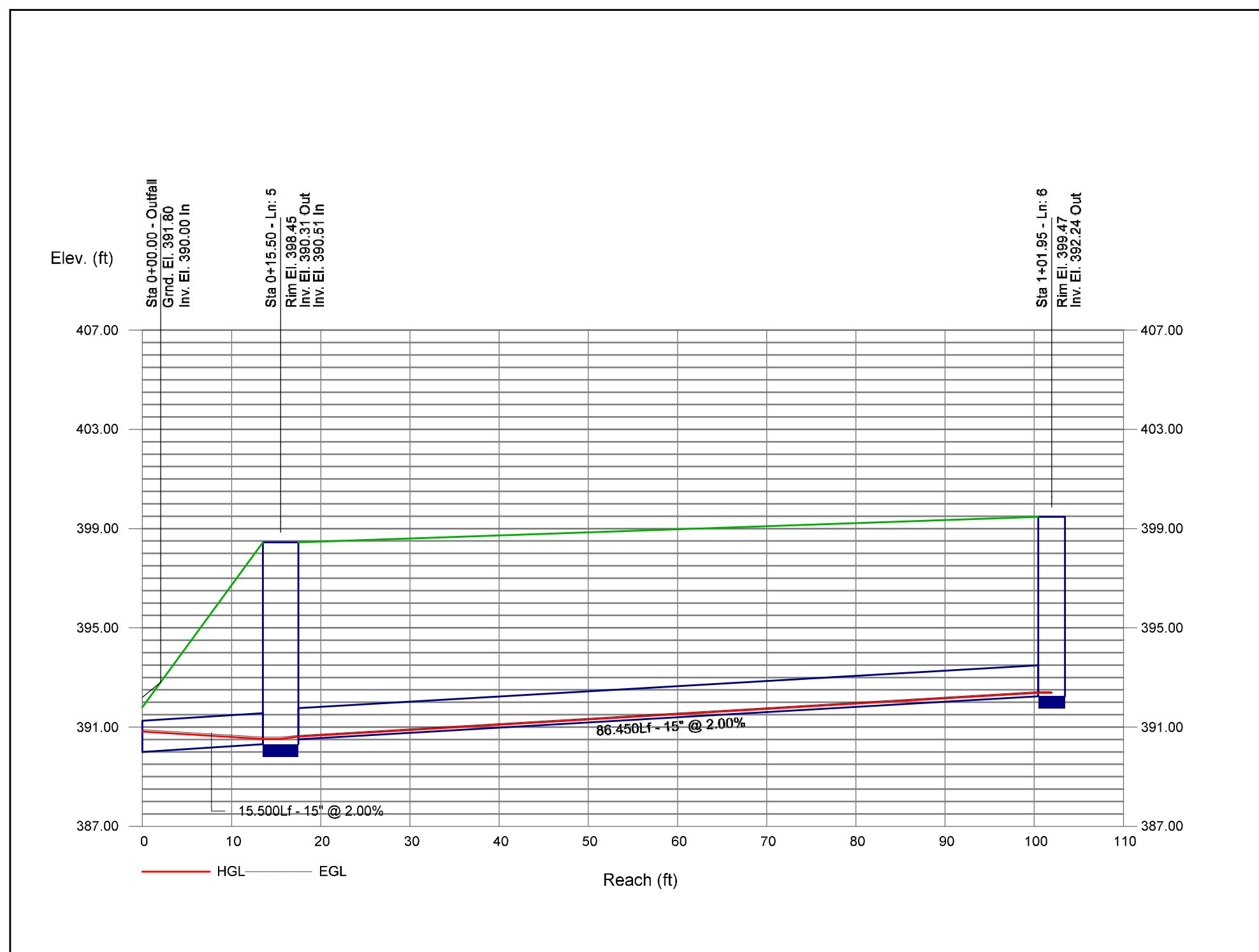
# Storm Sewer Profile

Proj. file: 2025-03-03 - Lot 8A HoF.stm



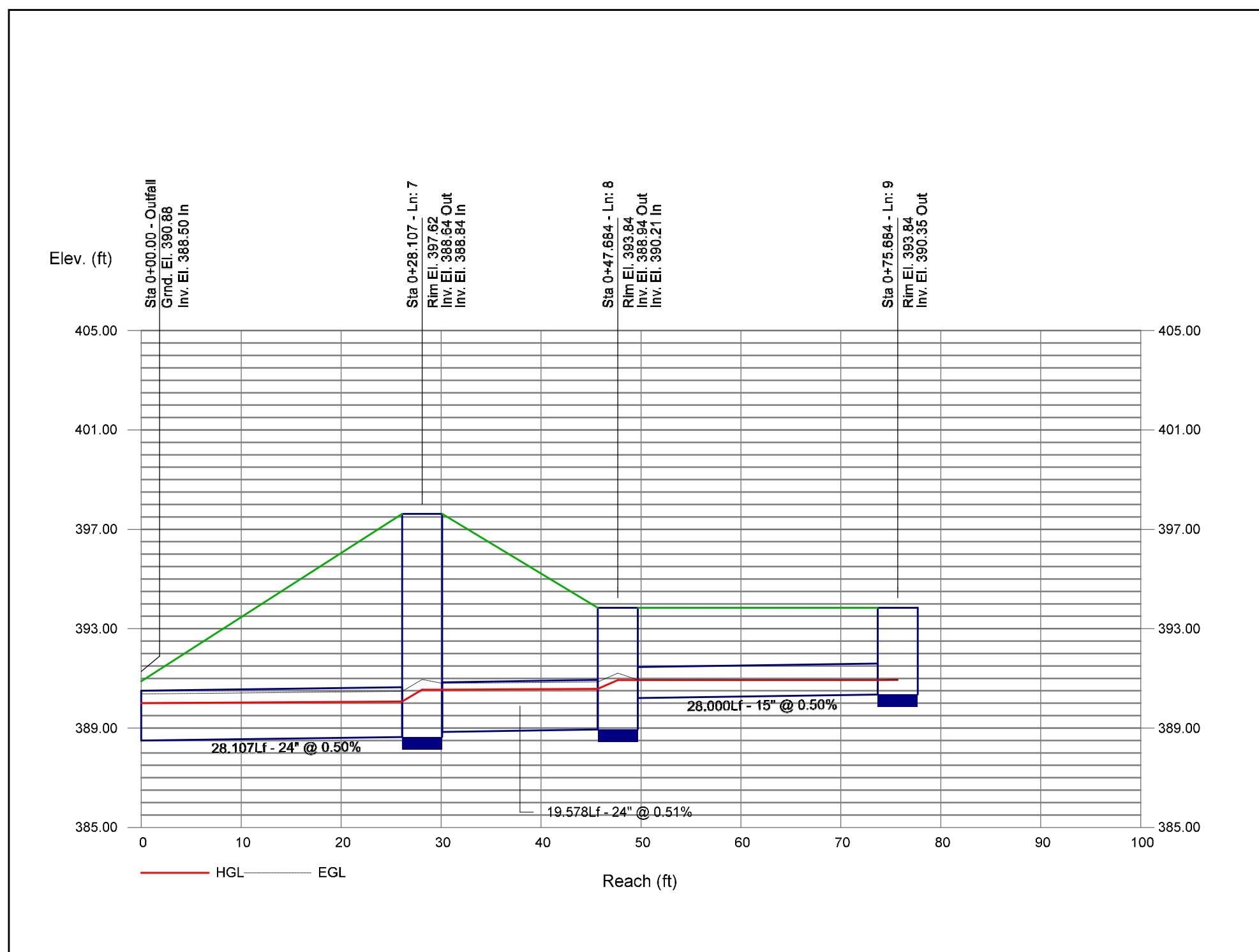
# Storm Sewer Profile

Proj. file: 2025-03-03 - Lot 8A HoF.stm



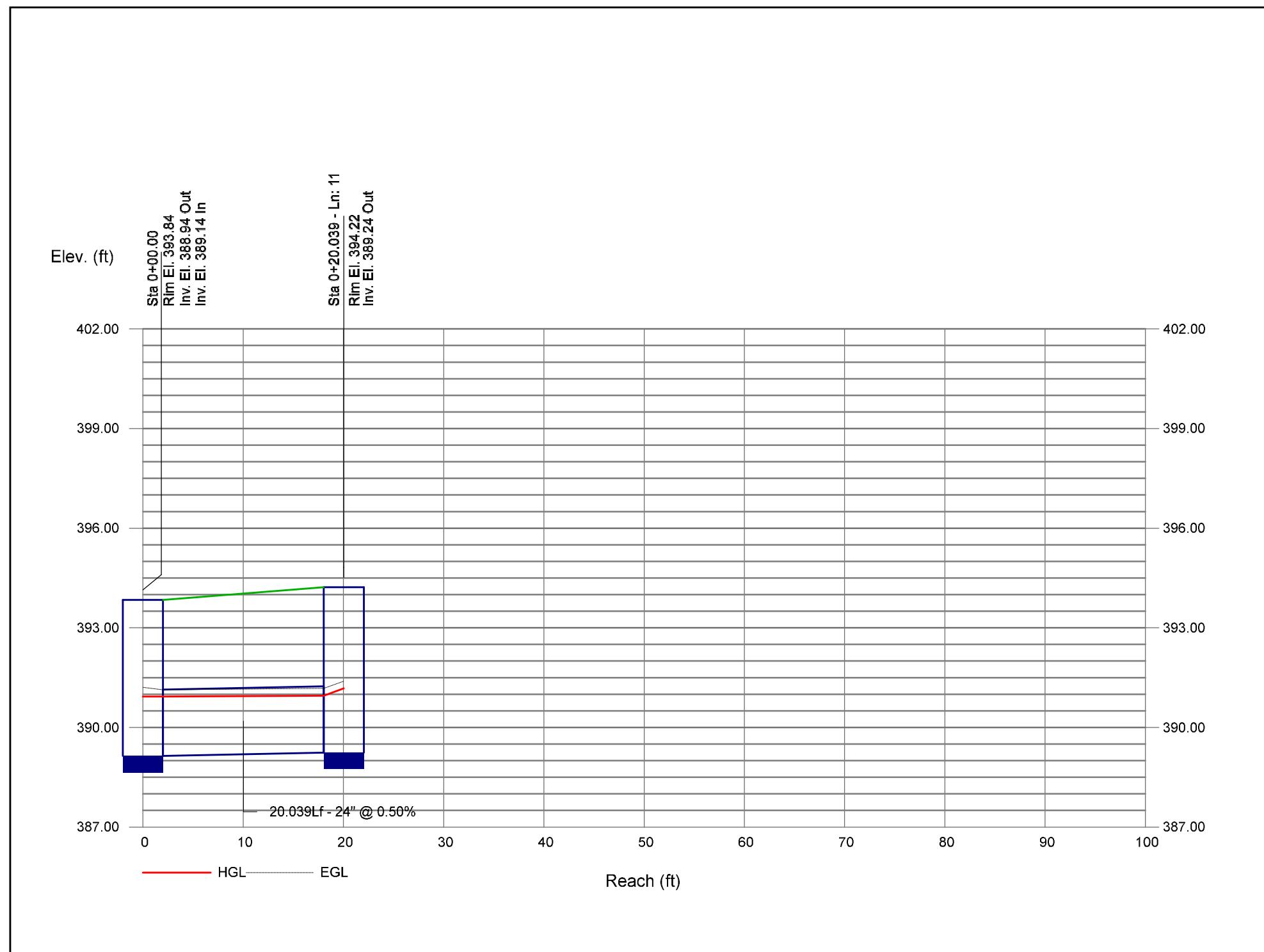
# Storm Sewer Profile

Proj. file: 2025-03-03 - Lot 8A HoF.stm



# Storm Sewer Profile

Proj. file: 2025-03-03 - Lot 8A HoF.stm



# Storm Sewer Profile

Proj. file: 2025-03-03 - Lot 8A HoF.stm

