

SITE DATA

| | | Project Information |
|--------------------|--|---|
| | Broject Name | Walibrook |
| | Project Name: Applicant: | |
| | Applicant. Applicant Contact Name: | Ben Mayo |
| | | Ben Mayo 919-361-5000 |
| | Applicant Contact Number: Contact Email: | montes@Mcadamsco.com |
| | Municipal Jurisdiction (Select from dropdown menu): | Rolesville |
| | Last Updated: | Monday, April 1, 2024 |
| | Last opuated. | |
| | | Site Data: |
| | Total Site Area (Ac): | 42.35 |
| | Existing Lake/Pond Area (Ac): | 0.00 |
| | Proposed Disturbed Area (Ac): | 18.50 |
| | Impervious Surface Area (acre): | 12.47 |
| | Type of Development (Select from Dropdown menu): | Residential |
| | Percent Built Upon Area (BUA): | 29% |
| | Project Density: | High |
| | Is the proposed project a site expansion? | No |
| ļ, | Number of Drainage Areas on Site: | 2 |
| | 1-Year, 24-Hour Storm (inches) (See NOAA Website): | 2.86 |
| NOAA | 2-Year, 24-Hour Storm (inches) (See NOAA Website): | 3.46 |
| | 10-Year, 24-Hour Storm (inches) (See NOAA Website): | 5.04 |
| | | Lot Data (if applicable): |
| | Total Acreage in Lots: | 8.15 |
| | Number of Lots: | 140 |
| | Average Lot Size (SF): | 2535.00 |
| | Total Impervious Surface Area on Lots (SF): | 226202.00 |
| | Average Impervious Surface Area Per Lot (SF): | 1615.73 |
| | Stormwater Narrative (limit to 1,200 |) characters - attach additional pages with submittal if necessary): |
| Impact Analysis in | cludes the development of the residential and one commercial | ated between Highway 401 and Wall Creek Drive. The development is approximately 43 acres. This Stormwater barcel. The proposed development on this site consists of the construction of 140 townhome units, along with her supporting infrastructure. For more detail see the Stormwater Calculations book. |
| | | |

Wallbrook



DRAINAGE AREA 1 STORMWATER PRE-POST CALCULATIONS

| LAND USE & SITE DATA | Р | RE-DEVE | | ΝT | PC | OST-DEV | ELOPME | NT | |
|---|--------------------------------|---------|------|-------|---------------------|---------|--------|------|--|
| Drainage Area (Acres)= | | 38 | .31 | | | 37 | .75 | | |
| Site Acreage within Drainage= | | 18 | .19 | | | 17 | .64 | | |
| One-year, 24-hour rainfall (in)= | | | | 2. | 86 | | | | |
| Two-year, 24-hour rainfall (in)= | | | | 3. | 46 | | | | |
| Ten-year, 24-hour storm (in)= | | | | 5. | 04 | | | | |
| Total Lake/Pond Area (Acres)= | | 0. | 00 | | | 0. | 23 | | |
| Lake/Pond Area not in the Tc flow path (Acres)= | | 0. | 00 | | | 0. | 23 | | |
| Site Land Use (acres): | А | В | С | D | А | В | С | D | |
| Pasture | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |
| Woods, Poor Condition | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |
| Woods, Fair Condition | 0.00 | 0.00 | 9.81 | 11.67 | 0.00 | 0.00 | 6.71 | 2.14 | |
| Woods, Good Condition | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |
| Open Space, Poor Condition | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |
| Open Space, Fair condition | 0.00 | 0.00 | 0.00 | 10.79 | 0.00 | 0.00 | 2.56 | 1.43 | |
| Open Space, Good Condition | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |
| Reforestation (in dedicated OS) | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |
| Connected Impervious | 0.00 | 0.00 | 0.22 | 5.79 | 0.00 | 0.00 | 2.57 | 2.23 | |
| Disconnected Impervious | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |
| SITE FLOW | PRE-DEVELOPMENT T _c | | | | POST-DEVELOPMENT Tc | | | | |
| Sheet Flow | | | | | | | | | |
| Length (ft)= | | 100 | 0.00 | | | | | | |
| Slope (ft/ft)= | | 0.0 |)40 | | | | | | |
| Surface Cover: | | Gr | ass | | | | | | |
| n-value= | | 0.2 | 240 | | | | | | |
| T _t (hrs)= | | 0.1 | 191 | | | | | | |
| Shallow Flow | | | | | | | | | |
| Length (ft)= | | 710 | 0.00 | | | | | | |
| Slope (ft/ft)= | | 0.0 |)31 | | | | | | |
| Surface Cover: | | Unp | aved | | | | | | |
| Average Velocity (ft/sec)= | | 2. | 84 | | | | | | |
| T _t (hrs)= | | 0. | 07 | | | | | | |
| Channel Flow 1 | | | | | | | | | |
| Length (ft)= | | 162 | 7.00 | | | | | | |
| Slope (ft/ft)= | | 0.0 |)23 | | | | | | |
| Cross Sectional Flow Area (ft ²)= | | 10 | .50 | | | | | | |
| Wetted Perimeter (ft)= | | 9. | 50 | | | | | | |
| Channel Lining: | | We | eds | | | | | | |
| n-value= | | 0.0 |)40 | | | | | | |
| Hydraulic Radius (ft)= | ft)= 1.11 | | | | | | | | |
| Average Velocity (ft/sec)= | | 6. | 09 | | | #VA | LUE! | | |
| T _t (hrs)= | | 0. | 07 | | | #VA | LUE! | | |



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DRAINAGE AREA 1 STORMWATER PRE-POST CALCULATIONS

| Channel Flow 2 | | |
|--|---|---|
| Length (ft)= | 0.00 | |
| Slope (ft/ft)= | 0.000 | |
| Cross Sectional Flow Area (ft ²)= | 0.00 | |
| Wetted Perimeter (ft)= | 0.00 | |
| Channel Lining: | 0.00 | |
| n-value= | | |
| Hydraulic Radius (ft)= | | |
| Average Velocity (ft/sec)= | | #VALUE! |
| T _t (hrs)= | | #VALUE! |
| Channel Flow 3 | | #VALUE! |
| | 0.00 | |
| Length (ft)= | | |
| Slope (ft/ft)= | 0.000 | |
| Cross Sectional Flow Area (ft ²)= | 0.00 | |
| Wetted Perimeter (ft)= | 0.00 | |
| Channel Lining: | | |
| n-value= | | |
| Hydraulic Radius (ft)= | | |
| Average Velocity (ft/sec)= | | #VALUE! |
| T _t (hrs)= | | #VALUE! |
| Tc (hrs)= | 0.33 | 0.08 |
| | | |
| | PRE-DEVELOPMENT | POST-DEVELOPMENT |
| Composite Curve Number= | PRE-DEVELOPMENT 82 | POST-DEVELOPMENT 82 |
| Composite Curve Number= Disconnected Impervious Adjustment | | |
| Composite Curve Number= Disconnected Impervious Adjustment Disconnected impervious area (acre) = | 82 | 82 |
| Composite Curve Number= Disconnected Impervious Adjustment Disconnected impervious area (acre) = CN _{adjusted (1-year)} = | | 82 |
| Composite Curve Number= Disconnected Impervious Adjustment Disconnected impervious area (acre) = CN _{adjusted (1-year)} = High Density Only | 82 | 82 |
| Composite Curve Number= Disconnected Impervious Adjustment Disconnected impervious area (acre) = CN _{adjusted (1-year)} = High Density Only Volume of runoff from 1" rainfall for DA | 82 | 82 |
| Composite Curve Number= Disconnected Impervious Adjustment Disconnected impervious area (acre) = CN _{adjusted (1-year)} = High Density Only Volume of runoff from 1" rainfall for DA HIGH DENSITY REQUIREMENT = (ft ³) = | 82 | 82 |
| Composite Curve Number= Disconnected Impervious Adjustment Disconnected impervious area (acre) = CN _{adjusted} (1-year)= High Density Only Volume of runoff from 1" rainfall for DA HIGH DENSITY REQUIREMENT = (ft ³) = 1-year, 24-hour storm (Peak Flow) | 82 | 82 |
| Composite Curve Number= Disconnected Impervious Adjustment Disconnected impervious area (acre) = CN _{adjusted (1-year} = High Density Only Volume of runoff from 1" rainfall for DA HIGH DENSITY REQUIREMENT = (ft ³) = 1-year, 24-hour storm (Peak Flow) Runoff (inches) = Q* _{1-year} = | 82 8 22, | 82 2 533 |
| Disconnected Impervious Adjustment Disconnected impervious area (acre) = CN _{adjusted (1-year)} = High Density Only Volume of runoff from 1" rainfall for DA HIGH DENSITY REQUIREMENT = (ft ³) = 1-year, 24-hour storm (Peak Flow) | 82 8 22, 1.26 | 82 2 533 1.29 |
| Composite Curve Number= Disconnected Impervious Adjustment Disconnected impervious area (acre) = CNadjusted (1-year)= High Density Only Volume of runoff from 1" rainfall for DA HIGH DENSITY REQUIREMENT = (ft ³) = 1-year, 24-hour storm (Peak Flow) Runoff (inches) = Q*1-year= Volume of runoff (ft ³) = | 82 8 22, 1.26 | 82 2 533 1.29 |
| Composite Curve Number= Disconnected Impervious Adjustment Disconnected impervious area (acre) = CN _{adjusted} (1-year)= High Density Only Volume of runoff from 1" rainfall for DA HIGH DENSITY REQUIREMENT = (ft ³) = 1-year, 24-hour storm (Peak Flow) Runoff (inches) = Q* _{1-year} = Volume of runoff (ft ³) = | 82 8 22, 1.26 83,207 | 82 2 533 1.29 82,497 |
| Composite Curve Number= Disconnected Impervious Adjustment Disconnected impervious area (acre) = CNadjusted (1-year)= High Density Only Volume of runoff from 1" rainfall for DA HIGH DENSITY REQUIREMENT = (ft ³) = 1-year, 24-hour storm (Peak Flow) Runoff (inches) = Q* _{1-year} = Volume of runoff (ft ³) = Volume change (ft ³) = Peak Discharge (cfs)= Q _{1-year} = | 82 8 22, 1.26 83,207 | 82 2 533 1.29 82,497 |
| Composite Curve Number= Disconnected Impervious Adjustment Disconnected impervious area (acre) = CN _{adjusted (1-year)} = High Density Only Volume of runoff from 1" rainfall for DA HIGH DENSITY REQUIREMENT = (ft ³) = 1-year, 24-hour storm (Peak Flow) Runoff (inches) = Q* _{1-year} = Volume of runoff (ft ³) = Volume change (ft ³) = Peak Discharge (cfs) = Q _{1-year} = 2-year, 24-hour storm (LID) | 82 8 22, 1.26 83,207 48.570 | 82 2 533 1.29 82,497 70.269 |
| Composite Curve Number= Disconnected Impervious Adjustment Disconnected impervious area (acre) = CN _{adjusted} (1-year)= High Density Only Volume of runoff from 1" rainfall for DA HIGH DENSITY REQUIREMENT = (ft ³) = 1-year, 24-hour storm (Peak Flow) Volume of runoff (inches) = Q* _{1-year} = Volume change (ft ³) = Peak Discharge (cfs) = Q _{1-year} = 2-year, 24-hour storm (LID) Runoff (inches) = Q* _{2-year} = | 82 8 22, 1.26 83,207 48.570 1.74 | 82 2 533 1.29 82,497 70.269 1.77 |
| Composite Curve Number= Disconnected Impervious Adjustment Disconnected Impervious area (acre) = CN _{adjusted (1-year)} = High Density Only Volume of runoff from 1" rainfall for DA HIGH DENSITY REQUIREMENT = (ft ³) = 1-year, 24-hour storm (Peak Flow) Volume of runoff (inches) = Q* _{1-year} = Volume change (ft ³) = Peak Discharge (cfs) = Q _{1-year} = 2-year, 24-hour storm (LID) Runoff (inches) = Q* _{2-year} = Volume of runoff (ft ³) = | 82 8 22, 1.26 83,207 48.570 1.74 114,793 | 82 2 533 1.29 82,497 70.269 70.269 1.77 113,421 |
| Composite Curve Number= Disconnected Impervious Adjustment Disconnected Impervious area (acre) = CN _{adjusted (1-year)} = High Density Only Volume of runoff from 1" rainfall for DA HIGH DENSITY REQUIREMENT = (ft ³) = 1-year, 24-hour storm (Peak Flow) Volume of runoff (inches) = Q* _{1-year} = Volume change (ft ³) = Peak Discharge (cfs)= Q _{1-year} = 2-year, 24-hour storm (LID) Runoff (inches) = Q* _{2-year} = Volume of runoff (ft ³) = | 82 8 22, 1.26 83,207 48.570 1.74 114,793 | 82 2 533 1.29 82,497 70.269 70.269 1.77 113,421 |
| Composite Curve Number Disconnected Impervious Adjustment Disconnected Impervious area (acre) = CN _{adjusted (1-year)} = High Density Only Volume of runoff from 1" rainfall for DA HIGH DENSITY REQUIREMENT = (ft ³) = 1-year, 24-hour storm (Peak Flow) Volume of runoff (finches) = Q* _{1-year} = Volume change (ft ³) = Peak Discharge (cfs) = Q _{1-year} = 2-year, 24-hour storm (LID) Runoff (inches) = Q* _{2-year} = Volume of runoff (ft ³) = Peak Discharge (cfs) = Q _{2-year} = Volume of runoff (ft ³) = Peak Discharge (cfs) = Q _{2-year} = 10-year, 24-hour storm (DIA) | 82 8 22, 1.26 83,207 48.570 1.74 1.74 114,793 67.007 | 82 2 533 1.29 82,497 70.269 70.269 1.77 113,421 96.610 |
| Composite Curve Number= Disconnected Impervious Adjustment Disconnected Impervious area (acre) = CN _{adjusted (1-year)} = High Density Only Volume of runoff from 1" rainfall for DA HIGH DENSITY REQUIREMENT = (ft ³) = 1-year, 24-hour storm (Peak Flow) Runoff (inches) = Q* _{1-year} = Volume of runoff (ft ³) = Peak Discharge (cfs) = Q _{1-year} = 2-year, 24-hour storm (LID) Runoff (inches) = Q* _{2-year} = Volume of runoff (ft ³) = Peak Discharge (cfs) = Q _{2-year} = Volume of runoff (ft ³) = Peak Discharge (cfs) = Q _{2-year} = 10-year, 24-hour storm (DIA) Runoff (inches) = Q* _{10-year} = | 82 8 22, 1.26 83,207 48.570 1.74 114,793 67.007 3.10 | 82 2 533 1.29 82,497 70.269 70.269 1.77 113,421 96.610 3.14 |

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DRAINAGE AREA 2 STORMWATER PRE-POST CALCULATIONS

| LAND USE & SITE DATA | Р | RE-DEVE | | ΙТ | PC | OST-DEV | ELOPME | NT | |
|---|--------|---------|-------|------------------|---------------------|---------|--------|------|--|
| Drainage Area (Acres)= | | 32 | .45 | | | 33 | .00 | | |
| Site Acreage within Drainage= | - | 24 | .15 | | | 24 | .70 | | |
| One-year, 24-hour rainfall (in)= | | | | 2. | 86 | | | | |
| Two-year, 24-hour rainfall (in)= | | | | 3. | 46 | | | | |
| Ten-year, 24-hour storm (in)= | | | | 5. | 04 | | | | |
| Total Lake/Pond Area (Acres)= | | 0. | 00 | | | 0. | 31 | | |
| Lake/Pond Area not in the Tc flow path (Acres)= | | 0. | 00 | | | 0. | 00 | | |
| Site Land Use (acres): | A | В | С | D | А | В | С | D | |
| Pasture | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |
| Woods, Poor Condition | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |
| Woods, Fair Condition | 0.00 | 0.00 | 17.92 | 6.23 | 0.00 | 0.00 | 6.43 | 2.43 | |
| Woods, Good Condition | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |
| Open Space, Poor Condition | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |
| Open Space, Fair condition | 0.00 | 0.00 | 0.00 | 2.35 | 0.00 | 0.00 | 5.38 | 2.81 | |
| Open Space, Good Condition | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |
| Reforestation (in dedicated OS) | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |
| Connected Impervious | 0.00 | 0.00 | 0.26 | 0.81 | 0.00 | 0.00 | 7.10 | 0.55 | |
| Disconnected Impervious | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |
| SITE FLOW | PR | E-DEVEL | OPMEN | Г Т _с | POST-DEVELOPMENT Tc | | | | |
| Sheet Flow | | | | | | | | | |
| Length (ft)= | | 100 | 0.00 | | | | | | |
| Slope (ft/ft)= | | 0.0 |)40 | | | | | | |
| Surface Cover: | | Wa | ods | | | | | | |
| n-value= | | 0.4 | 100 | | | | | | |
| T _t (hrs)= | | 0.2 | 287 | | | | | | |
| Shallow Flow | | | | | | | | | |
| Length (ft)= | | 134 | 5.00 | | | | | | |
| Slope (ft/ft)= | | 0.0 |)33 | | | | | | |
| Surface Cover: | | Unp | aved | | | | | | |
| Average Velocity (ft/sec)= | | 2. | 92 | | | | | | |
| T _t (hrs)= | | 0. | 13 | | | | | | |
| Channel Flow 1 | | | | | | | | | |
| Length (ft)= | | 122 | 1.00 | | | | | | |
| Slope (ft/ft)= | | 0.0 |)21 | | | | | | |
| Cross Sectional Flow Area (ft ²)= | | 10 | .50 | | | | | | |
| Wetted Perimeter (ft)= | | 9. | 50 | | | | | | |
| Channel Lining: | | We | eds | | | | | | |
| n-value= | | 0.0 |)40 | | | | | | |
| Hydraulic Radius (ft)= | = 1.11 | | | | | | | | |
| Average Velocity (ft/sec)= | | 5. | 81 | | | | | | |
| T _t (hrs)= | | 0. | 06 | | | | | | |



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DRAINAGE AREA 2 STORMWATER PRE-POST CALCULATIONS

| Channel Flow 2 Length (ft)= Slope (ft/ft)= | |
|--|-------|
| Slope (ft/ft)= | |
| | |
| Cross Sectional Flow Area (ft ²)= | |
| Wetted Perimeter (ft)= | |
| Channel Lining: | |
| n-value= | |
| Hydraulic Radius (ft)= | |
| Average Velocity (ft/sec)= | |
| T, (hrs)= | |
| Channel Flow 3 | |
| Length (ft)= | |
| Slope (ft/ft)= | |
| Cross Sectional Flow Area (ft ²)= | |
| | |
| Wetted Perimeter (ft)= Channel Lining: | |
| n-value= | |
| Hydraulic Radius (ft)= | |
| Average Velocity (ft/sec)= | |
| T _t (hrs)= | |
| Tc (hrs)= 0.47 0.08 | |
| RESULTS PRE-DEVELOPMENT POST-DEVELOPME | |
| | |
| Composite Curve Number= 76 84 | _1111 |
| | |
| Composite Curve Number= 76 84 | |
| Composite Curve Number= 76 84 Disconnected Impervious Adjustment | |
| Composite Curve Number= 76 84 Disconnected Impervious Adjustment Disconnected impervious area (acre) = | |
| Composite Curve Number= 76 84 Disconnected Impervious Adjustment Disconnected impervious area (acre) = CN _{adjusted (1-year)} = 84 | _11 1 |
| Composite Curve Number= 76 84 Disconnected Impervious Adjustment | |
| Composite Curve Number= 76 84 Disconnected Impervious Adjustment 5 Disconnected impervious area (acre) = CNadjusted (1-year) 84 High Density Only 84 Volume of runoff from 1" rainfall for DA HIGH DENSITY REQUIREMENT = (ft ³) = 30,982 | |
| Composite Curve Number= 76 84 Disconnected Impervious Adjustment Disconnected impervious area (acre) = CN _{adjusted} (1-year) ⁼ 84 High Density Only 84 Volume of runoff from 1" rainfall for DA HIGH DENSITY REQUIREMENT = (ft ³) = 30,982 1-year, 24-hour storm (Peak Flow) | |
| Composite Curve Number= 76 84 Disconnected Impervious Adjustment | |
| Composite Curve Number= 76 84 Disconnected Impervious Adjustment Disconnected impervious area (acre) = CN _{adjusted} (1-year) ⁼ Kigh Density Only Volume of runoff from 1" rainfall for DA HIGH DENSITY REQUIREMENT = (ft ³) = 1-year, 24-hour storm (Peak Flow) Runoff (inches) = Q*1-year ⁼ 0.94 Volume of runoff (ft ³) = 82,020 | |
| Composite Curve Number= 76 84 Disconnected Impervious Adjustment | |
| Composite Curve Number=7684Disconnected Impervious Adjustment I Disconnected impervious area (acre) = I CNadjusted (1-year) =84High Density Only I Volume of runoff from 1" rainfall for DA HIGH DENSITY REQUIREMENT = (ft ³) = $30,982$ 1-year, 24-hour storm (Peak Flow) 1.39 Volume of runoff (inches) = Q^*_{1-year} 0.94 1.39 Volume of runoff (ft ³) = $82,020$ $125,024$ Volume change (ft ³) = $43,004$ 16418 | |
| Composite Curve Number= 76 84 Disconnected Impervious Adjustment | |
| Composite Curve Number=7684Disconnected Impervious Adjustment I Disconnected impervious area (acre) = I CNadjusted (1-year)=84High Density Only I Volume of runoff from 1" rainfall for DA HIGH DENSITY REQUIREMENT = (ft 3) = 30.982 1-year, 24-hour storm (Peak Flow) 1.39 Volume of runoff (inches) = Q*_{1-year}= 0.94 1.39 Volume change (ft 3) = 43.004 125.024Volume change (ft 3) = 21.448 76.4182-year, 24-hour storm (LID) 1.35 1.89 | |
| Composite Curve Number=7684Disconnected Impervious Adjustment $1000000000000000000000000000000000000$ | |
| Composite Curve Number=7684Disconnected Impervious Adjustment $1000000000000000000000000000000000000$ | |
| Composite Curve Number=7684Disconnected Impervious Adjustment 76 84Disconnected Impervious area (acre) = $CN_{adjusted (1-year)}$ 84 CN_{adjusted (1-year)} 84 High Density Only $30,982$ Volume of runoff from 1* rainfall for DA HIGH DENSITY REQUIREMENT = (ft ³) = $30,982$ 1-year, 24-hour storm (Peak Flow) $30,982$ Volume of runoff (inches) = Q^*_{1-year} 0.94 1.39 Volume of runoff (ft ³) = $82,020$ $125,024$ Volume change (ft ³) = $43,004$ 76.418 2-year, 24-hour storm (LiD) 1.35 1.89 Numoff (inches) = Q^*_{2-year} 1.35 1.89 Quiume of runoff (ft ³) = $118,608$ $169,788$ Peak Discharge (cfs) = Q_{2-year} 31.016 103.780 10-year, 24-hour storm (DIA) $10-year, 24-hour storm (DIA)$ | |



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DA SITE SUMMARY STORMWATER PRE-POST CALCULATIONS

| | | SITE | SUMMAR | (| | | | | | | |
|--|----------------|---------------------------------|---|-------------------------|--------|-----------------|------|-----|-------------|------|--|
| DRAINAGE AREA SUMMARIES | | | | | | | | | | | |
| DRAINAGE AREA: | DA1 | DA2 | DA3 | DA4 | DA5 | DA6 | DA7 | DA8 | DA9 | DA10 | |
| Pupoff (in) = 0 | | | (1-year, 24- | hour stor | m) | | | | 1 | | |
| Runoff (in) = Q _{pre,1-year} = Peak Flow (cfs)=Q _{1-year} = | 1.26 48.570 | 0.94 21.448 | | | | | | | | | |
| Peak Flow (CIS)-Q _{1-year} - | | | (1-year, 24 | -hour stor | (m) | | | | | | |
| Proposed Impervious Surface (acre) = | 4.80 | 7.65 | (1-year, 24 | -11001 3101 | , | I | I | | 1 | | |
| Runoff (in)=Q _{1-year} = | 1.29 | 1.39 | | | | | | | | | |
| Peak Flow (cfs)=Q _{1-year} = | 70.269 | 76.418 | | | | | | | | | |
| Increase in volume per DA (ft ³)_1-yr storm= | 10.203 | 43,004 | | | | | | | | | |
| Minimum Volume to be Managed for DA | 22,533 | 30,982 | | | | | | | | | |
| HIGH DENSITY REQUIREMENT = (ft ³) = TARGET CURVE NUMBER (TCN) | | | | | | | | | | | |
| , | | Si | te Data | | | | | | | | |
| | | | COMPOSI | TION | | | | | | | |
| HYDROLOGIC SOIL GROU | JP | | | Site | Area | | % | | Target CN | 1 | |
| A | | | | | 00 | | 1% | | N/A | - | |
| В | | | | 0. | 00 | C | 1% | | N/A | | |
| С | | | 30 | .75 | 7 | 3% | | N/A | | | |
| D | | | 11 | .59 | 27% | | | N/A | | | |
| | То | tal Site Area | (acres) = | | | 42 | 2.34 | | | | |
| Percent BU | JA (Include | es Existing Lakes/Pond Areas) = | | | | 29% | | | | | |
| | | Project Density = | | | | High | | | | | |
| | | Target Curve Number (TCN) = | | | N/A | | | | | | |
| | | | CN _{adju} | sted (1-year)= | | · · · | | | | | |
| Minimum Volume to be Manage | ed (Total S | Site) Per TO | N Requirer | nent= ft ³ = | | | | | | | |
| | s | ite Nitrog | en Loading | Data | | | | | | | |
| HSG | | | TN export coefficient (lbs/ac/yr) | | | Site Acreage | | | N Export | | |
| Pasture | | | 1.2 | | | 0.00 | | | 0.00 | | |
| Woods, Poor Condition | | | 1.6 | | | 0.00 | | | 0.00 | | |
| Woods, Fair Condition | | | 1.2 | | | 17.71 | | | 21.25 | | |
| Woods, Good Condition | | | 0.8 | | | 0.00 | | | 0.00 | | |
| Open Space, Poor Condition | | | 1.0 | | | 0.00 | | | 0.00 | | |
| Open Space, Fair Condition | | | 0.8 | | | 12.18 | | | 9.74 | | |
| Open Space, Good Condition | | | 0.6 | | | 0.00 | | | 0.00 | | |
| Reforestation (in dedicated OS) | | | 0.6 | | | 0.00 | | | 0.00 | | |
| Impervious | | | 21.2 | | | 12.45 | | | 263.94 | | |
| SITE NITROGEN LOADING RATE (I | bs/ac/yr)= | | | | | 6.97 | | | | | |
| Nitrogen Load | | | | | | 294.94 | | | | | |
| TOTAL SITE NITROGEN TO MITIGATE (lbs/yr)_Wend | dell Only= | | | | | 142.51 | | | | | |
| Sit | te Nitroge | n Loading | Data For E | xpansion | s Only | | | | | | |
| | | | Existing | | | | | New | | | |
| Impervious(acres)= | | | NA | | | | | NA | | | |
| "Expansion Area" (acres=) | | | | | | 1 | | | | | |
| Nitrogen Load (lbs/yr)= | | | NA | | | | | NA | | | |
| SITE NITROGEN LOADING RATE (lbs/ac/yr)= | | | NA | | | | | NA | | | |
| Total Site loading rate (lbs/ac/yr) | | | | | | | | | | | |
| TOTAL SITE NITROGEN TO MITIGATE (lbs/yr)= | | | | | N/ | A | | | | | |



Wallbrook

DRAINAGE AREA 1 BMP CALCULATIONS

| DRAINAGE AREA 1 - BMP DEVICES AN | ID ADJUSTMENTS | | | | | | | | | | |
|--|--|---|-------------------------------|-------|--|---|--------------|-----------------------------------|-----------------------------|------------------------------|-----------------------------|
| DA1 Site Acreage= | | | | 17.6 | 4 | | | | | | |
| DA1 Off-Site Acreage= | | | | 20.1 | 1 | | | | | | |
| Total Required Storage Volume for Site | | | | | | | | | | | |
| TCN Requirement (ft ³)= Total Required Storage Volume for DA1 | | | | | | | | | | | |
| 1" Rainfall for High Density (ft ³)= | | | | 22,53 | 33 | | | | | | |
| Will site use underground detention/cistern? | No | Enter % of the year water will be reused= | | 0% | | Note: Supporting information/details shou submitted to demonstrate water usage. | | | | | |
| ENTER ACREAGE FOR ALL SUB-DRAINAGE | AREAS IN DA | | | | | | | | | | |
| | HSG | Sub-DA1(a) Sub-DA (Ac) (Ac) Site Off-site Site | | | | Sub-DA1(d) (Ac) Site Off-site | | | DA1(e) Ac) Off-site | | |
| Pasture | | 0110 | 0.01 | Cito | OII OILO | Gillo | | - Child | OII OILO | Gito | |
| Woods, Poor Condition | | | | | | | | | | | |
| Woods, Fair Condition | | | | 8.85 | 4.84 | | | | | | |
| Woods, Good Condition | | | | | | | | | | | |
| Open Space, Poor Condition | | | | | | | | | | | |
| Open Space, Fair Condition | | 2.32 | | 1.67 | 9.85 | | | | | | |
| Open Space, Good Condition | | | | | | | | | | | |
| Reforestation (in dedicated OS) | | | | | | | | | | | |
| Impervious | | 4.80 | 0.01 | | 5.41 | | | | | | |
| Sub-DA1(a) BMP(s) | | 4.00 | 0.01 | | 0.41 | | | | | | |
| Device Name (As Shown on Plan) | Device Type | | er Quality Vo or Sub-DA (f | | Provided Volume that will <u>drawdown 2-5 days</u> (ft ³) | | | Nitrogen Removal Efficiency | Sub-DA Nitrogen (Ibs) | Nitrogen Removed (Ibs) | Drawdown Time (hours) |
| SCM A | Wet Detention Basin | | | | | | | 25% | 103.84 | 25.96 | 53.76 |
| | | | | | | | | 0% | 77.88 | 0.00 | |
| | | | 4,267 | | | 16,901 | | 0% | 77.88 | 0.00 | |
| | | | | | | | | 0% | 77.88 | 0.00 | |
| | | | | | | | | 0% | 77.88 | 0.00 | |
| Τα | tal Nitrogen remaining leaving the subbasin (lbs): | | | | | 77 | .88 | | 1 | | |
| Sub-DA1(b) BMP(s) | | | | | | | | | | | |
| enter | If Sub-DA1(b) is connected to upstream subbasin(s), the nitrogen leaving the most upstream subbasin(lbs): | | | | | | | | | | |
| Device Name (As Shown on Plan) | Device Type | | er Quality Vo or Sub-DA (f | | | Provided /olume that v awdown 2-5 c (ft ³) | | Nitrogen Removal Efficiency | Sub-DA Nitrogen (Ibs) | Nitrogen Removed (Ibs) | Drawdown Time (hours) |
| Bypass | | | | | | | | 0% | 140.34 | 0.00 | |
| | | | | | | | | 0% | 140.34 | 0.00 | |
| | | | 19,890 | | | | | 0% | 140.34 | 0.00 | |
| | | | | | | | | 0% | 140.34 | 0.00 | |
| | | | | | | | | 0% | 140.34 | 0.00 | |
| Τα | tal Nitrogen remaining leaving the subbasin (lbs): | | | | | 14 | 0.34 | | | | |
| Sub-DA1 (c) BMP(s) | | | | | | | | | | | |
| enter | If Sub-DA1(c) is connected to upstream subbasin(s), the nitrogen leaving the most upstream subbasin(lbs): | | | | | | | | | | |
| Device Name (As Shown on Plan) | Device Type | Water Quality Volume for Sub-DA (ft ³) | | | V <u>dra</u> | Provided /olume that v awdown 2-5 c (ft ³) | vill lays | Nitrogen Removal Efficiency | Sub-DA Nitrogen (Ibs) | Nitrogen Removed (Ibs) | Drawdown Time (hours) |
| | | | | | | | | 0% | 0.00 | 0.00 | |
| | | | | | | | | 0% | 0.00 | 0.00 | |
| | | | | | | | | 0% | 0.00 | 0.00 | |
| | | 1 | | | | | | 0% | 0.00 | 0.00 | |
| | | 1 | | | | | | 0% | 0.00 | 0.00 | |
| То | tal Nitrogen remaining leaving the subbasin (lbs): | | | | | | | | • | | |



Wallbrook

DRAINAGE AREA 1 BMP CALCULATIONS

| Sub-DA1(d) BMP(s) | | | | | | | | | | |
|---|---|---|--|-----------------------------------|-----------------------------|------------------------------|-----------------------------|--|--|--|
| | pasin(s), enter the nitrogen leaving the most upstream | | | | | | | | | |
| | subbasin(lbs): | | 1 | | | 1 | | | | |
| Device Name (As Shown on Plan) | Device Type | Water Quality Volume for Sub-DA (ft ³) | Provided Volume that will <u>drawdown 2-5 days</u> (ft ³) | Nitrogen Removal Efficiency | Sub-DA Nitrogen (Ibs) | Nitrogen Removed (Ibs) | Drawdown Time (hours) | | | |
| | | | | 0% | 0.00 | 0.00 | | | | |
| | | | | 0% | 0.00 | 0.00 | | | | |
| | | | | 0% | 0.00 | 0.00 | | | | |
| | | | | 0% | 0.00 | 0.00 | | | | |
| | | | | 0% | 0.00 | 0.00 | | | | |
| То | tal Nitrogen remaining leaving the subbasin (lbs): | | | | | | | | | |
| Sub-DA1(e) BMP(s) | | | | | | | | | | |
| If Sub-DA1(e) is connected to upstream subt | basin(s), enter the nitrogen leaving the most upstream subbasin(lbs): | | | 1 | | 1 | | | | |
| Device Name (As Shown on Plan) | Device Type | Water Quality Volume for Sub-DA (ft ³) | Provided Volume that will <u>drawdown 2-5 days</u> (ft ³) | Nitrogen Removal Efficiency | Sub-DA Nitrogen (Ibs) | Nitrogen Removed (Ibs) | Drawdown Time (hours) | | | |
| | | | | 0% | 0.00 | 0.00 | | | | |
| | | | | 0% | 0.00 | 0.00 | | | | |
| | | | | 0% | 0.00 | 0.00 | | | | |
| | | | | 0% | 0.00 | 0.00 | | | | |
| | | | | 0% | 0.00 | 0.00 | | | | |
| То | tal Nitrogen remaining leaving the subbasin (lbs): | | | | | | | | | |
| | DA | A1 BMP SUMMARY | | | | | | | | |
| | Total Volume Treated (ft ³)= | | 16,901 | | | | | | | |
| | Nitrogen Mitigated(Ibs)= | = 25.96 | | | | | | | | |
| 1-year, 24-hour storm | | | | | | | | | | |
| | Post BMP Volume of Runoff (ft ³) _(1-year) = | | 65,596 | | | | | | | |
| | Post BMP Runoff (inches) = Q* _(1-year) = | | 1.02 | | | | | | | |
| | Post BMP CN _(1-year) = | | 77 | | | | | | | |
| | Post BMP Peak Discharge (cfs)= Q _{1-year} = | | 36.440 | | | | | | | |
| 2-year, 24-hour storm (LID) | | | | | | | | | | |
| | Post BMP Volume of Runoff (ft3) _(2-year) = | | 96,520 | | | | | | | |
| | Post BMP Runoff (inches) = Q* _(2-year) = | | 1.51 | | | | | | | |
| | Post BMP CN _(2-year) = | | 78 | | | | | | | |
| | Post BMP Peak Discharge (cfs)= Q _(2-year) = | | 50.430 | | | | | | | |
| 10-year, 24-hour storm (DIA) | | | | | | | | | | |
| | Post BMP Volume of Runoff (ft ³) _(10-year) = | | 190,592 | | | | | | | |
| | Post BMP Runoff (inches) = Q* _(10-year) = | | 2.98 | | | | | | | |
| | Post BMP CN(10-year)= | | 95 | | | | | | | |
| | Post BMP Peak Discharge (cfs)= Q _(10-year) = | | 100.390 | | | | | | | |
| | | | | | | | | | | |



Wallbrook

DRAINAGE AREA 2 BMP CALCULATIONS

| DRAINAGE AREA 1 - BMP DEVICES AN | ND ADJUSTMENTS | | | | | | | | | | | |
|--|--|--|--------------------------------|-------|--|---|--------------|-------------------------------------|-----------------------------|------------------------------|-----------------------------|--|
| DA2 Site Acreage= | | | | 24.7 | 0 | | | | | | | |
| DA2 Off-Site Acreage= | | | | 8.30 |) | | | | | | | |
| Total Required Storage Volume | | | | | | | | | | | | |
| TCN Requirement (ft ³)= Total Required Storage Volume for DA2 | | | | | | | | | | | | |
| 1" Rainfall for High Density (ft3)= | | | | 30,98 | 32 | | | _ | | | | |
| Will site use underground detention/cistern? | No | Enter % of the year water will be reused= | | 0% | | Note: Supporting information/details should submitted to demonstrate water usage. | | | | | | |
| ENTER ACREAGE FOR ALL SUB-DRAINAGE | AREAS IN DA | 1 | | | | | | | | | | |
| | HSG | | DA2(a) ac) Off-site | | DA2(b) Sub-DA2(c) Ac) (Ac) Off-site Site Off-site | | lc) | Sub-DA2(d) (Ac) Site Off-site | | | DA2(e) Ac) Off-site | |
| Pasture | | - Child | Oll Ollo | 0.10 | OII OILO | Gillo | | Cito | Oll Gild | 0110 | Oll Ollo | |
| Woods, Poor Condition | | | | | | | | | | | | |
| Woods, Fair Condition | | | | 8.86 | 4.84 | | | | | | | |
| Woods, Good Condition | | | | | | | | | | | | |
| Open Space, Poor Condition | | | | | | | | | | | | |
| Open Space, Fair Condition | | 3.95 | | 4.29 | 9.85 | | | | | | | |
| Open Space, Good Condition | | | | | | | | | | | | |
| Reforestation (in dedicated OS) | | | | | | | | | | | | |
| Impervious | | 7.60 | | | 0.95 | | | | | | | |
| Sub-DA1(a) BMP(s) | | | | | | | | - | | | | |
| Device Name (As Shown on Plan) | Device Type | | er Quality Vo or Sub-DA (fl | | | Provided /olume that v awdown 2-5 c (ft ³) | | Nitrogen Removal Efficiency | Sub-DA Nitrogen (Ibs) | Nitrogen Removed (Ibs) | Drawdown Time (hours) | |
| SCM B | Wet Detention Basin | | | | | | | 25% | 164.28 | 41.07 | 51.84 | |
| | | | | | | | | 0% | 123.21 | 0.00 | | |
| | | | 9,205 | | | 26,929 | | 0% | 123.21 | 0.00 | | |
| | | | | | | | | 0% | 123.21 | 0.00 | | |
| | | | | | | | | 0% | 123.21 | 0.00 | | |
| Τα | tal Nitrogen remaining leaving the subbasin (lbs): | | | | | 12: | 3.21 | | | | | |
| Sub-DA1(b) BMP(s) | | | | | | | | | | | | |
| enter | If Sub-DA1(b) is connected to upstream subbasin(s), the nitrogen leaving the most upstream subbasin(lbs): | | | | P | | | 1 | 1 | P | 1 | |
| Device Name (As Shown on Plan) | Device Type | | er Quality Vo or Sub-DA (fl | | Provided Volume that will <u>drawdown 2-5 days</u> (ft ³) | | | Nitrogen Removal Efficiency | Sub-DA Nitrogen (Ibs) | Nitrogen Removed (Ibs) | Drawdown Time (hours) | |
| Bypass | | | | | | | | 0% | 47.89 | 0.00 | | |
| | | | | | | | | 0% | 47.89 | 0.00 | | |
| | | | 7,440 | | | | | 0% | 47.89 | 0.00 | | |
| | | | | | | | | 0% | 47.89 | 0.00 | | |
| | | | | | | | | 0% | 47.89 | 0.00 | | |
| То | tal Nitrogen remaining leaving the subbasin (lbs): | | | | | 47 | .89 | | | | | |
| Sub-DA1 (c) BMP(s) | | 1 | | | | | | | | | | |
| enter | If Sub-DA1(c) is connected to upstream subbasin(s), the nitrogen leaving the most upstream subbasin(lbs): | | | | T | | | 1 | I | T | I | |
| Device Name (As Shown on Plan) | Device Type | | er Quality Vo or Sub-DA (fi | | V <u>dra</u> | Provided /olume that v awdown 2-5 c (ft ³) | vill lays | Nitrogen Removal Efficiency | Sub-DA Nitrogen (Ibs) | Nitrogen Removed (Ibs) | Drawdown Time (hours) | |
| | | | | | | | | 0% | 0.00 | 0.00 | | |
| | | | | | | | | 0% | 0.00 | 0.00 | | |
| | | | | | | | | 0% | 0.00 | 0.00 | | |
| | | | | | | | | 0% | 0.00 | 0.00 | | |
| | | | | | | | | 0% | 0.00 | 0.00 | | |
| Τα | tal Nitrogen remaining leaving the subbasin (lbs): | | | | | | | | | | | |



Wallbrook

DRAINAGE AREA 2 BMP CALCULATIONS

| Sub-DA1(d) BMP(s) | | | | | | | | | | | |
|---|--|---|--|-----------------------------------|-----------------------------|------------------------------|-----------------------------|--|--|--|--|
| If Sub-DA1(d) is connected to upstream subb | asin(s), enter the nitrogen leaving the most upstream subbasin(lbs): | | | | | | | | | | |
| Device Name (As Shown on Plan) | Device Type | Water Quality Volume for Sub-DA (ft ³) | Provided Volume that will <u>drawdown 2-5 days</u> (ft ³) | Nitrogen Removal Efficiency | Sub-DA Nitrogen (Ibs) | Nitrogen Removed (Ibs) | Drawdown Time (hours) | | | | |
| | | | | 0% | 0.00 | 0.00 | | | | | |
| | | | | 0% | 0.00 | 0.00 | | | | | |
| | | | | 0% | 0.00 | 0.00 | | | | | |
| | | | | 0% | 0.00 | 0.00 | | | | | |
| | | | | 0% | 0.00 | 0.00 | | | | | |
| Tot | tal Nitrogen remaining leaving the subbasin (lbs): | | | | | | | | | | |
| Sub-DA1(e) BMP(s) | | | | | | | | | | | |
| If Sub-DA1(e) is connected to upstream subb | asin(s), enter the nitrogen leaving the most upstream subbasin(lbs): | | | | | | | | | | |
| Device Name (As Shown on Plan) | Device Type | Water Quality Volume for Sub-DA (ft ³) | Provided Volume that will <u>drawdown 2-5 days</u> (ft ³) | Nitrogen Removal Efficiency | Sub-DA Nitrogen (Ibs) | Nitrogen Removed (Ibs) | Drawdown Time (hours) | | | | |
| | | | | 0% | 0.00 | 0.00 | | | | | |
| | | | | 0% | 0.00 | 0.00 | | | | | |
| | | | | 0% | 0.00 | 0.00 | | | | | |
| | | | | 0% | 0.00 | 0.00 | | | | | |
| | | | | 0% | 0.00 | 0.00 | | | | | |
| Tot | tal Nitrogen remaining leaving the subbasin (lbs): | | | | | | | | | | |
| | DA | A2 BMP SUMMARY | | | | | | | | | |
| | Total Volume Treated (ft ³)= | | 26,929 | | | | | | | | |
| | Nitrogen Mitigated(Ibs)= |)= 41.07 | | | | | | | | | |
| 1-year, 24-hour storm | | | | | | | | | | | |
| | Post BMP Volume of Runoff (ft ³) _(1-year) = | | 98,095 | | | | | | | | |
| | Post BMP Runoff (inches) = $Q^*_{(1-year)}$ = | | 1.09 | | | | | | | | |
| | Post BMP CN _(1-year) = | | 79 | | | | | | | | |
| | Post BMP Peak Discharge (cfs)= Q _{1-year} = | | 18.750 | | | | | | | | |
| 2-year, 24-hour storm (LID) | | | | | | | | | | | |
| | Post BMP Volume of Runoff (ft3) _(2-year) = | | 142,859 | | | | | | | | |
| | Post BMP Runoff (inches) = Q* _(2-year) = | | 1.59 | | | | | | | | |
| | Post BMP CN _(2-year) = | | 79 | | | | | | | | |
| | Post BMP Peak Discharge (cfs)= Q _(2-year) = | | 27.240 | | | | | | | | |
| 10-year, 24-hour storm (DIA) | | | | | | | | | | | |
| | Post BMP Volume of Runoff (ft ³) _(10-year) = | | 262,042 | | | | | | | | |
| | Post BMP Runoff (inches) = Q* _(10-year) = | | 2.92 | | | | | | | | |
| | Post BMP CN(_{10-year})= | | 95 | | | | | | | | |
| | Post BMP Peak Discharge (cfs)= Q _(10-year) = | | 70.960 | | | | | | | | |
| | | | | | | | | | | | |



Wallbrook

DA SITE SUMMARY BMP CALCULATIONS

| | BN | IP SUMM | ARY | | | | | | | |
|--|----------|------------|--------------|-------|------|-----|-----|-----|-----|------|
| DRAINAGE AREA SUMMARIES | | | | | | | | | | |
| DRAINAGE AREA: | DA1 | DA2 | DA3 | DA4 | DA5 | DA6 | DA7 | DA8 | DA9 | DA10 |
| Pre- | Developm | ent (1-yea | r, 24-hour s | torm) | | | | | | |
| Runoff (in)=Q* _{1-year} = | 1.26 | 0.94 | | | | | | | | |
| Peak Flow (cfs)=Q _{1-year} = | 48.570 | 21.448 | | | | | | | | |
| Post-Development (1-year, 24-hour storm) | | | | | | | | | | |
| Target Curve Number (TCN) = | | | | | NA | | | | | |
| Post BMP Runoff (inches) = Q* _(1-year) = | 1.02 | 1.09 | | | | | | | | |
| Post BMP Peak Discharge (cfs)= Q _{1-year} = | 36.440 | 18.750 | | | | | | | | |
| Post BMP CN _(1-year) = | | | | | | | | | | |
| | Post-BN | IP Nitroge | n Loading | | | | | | | |
| TOTAL SITE NITROGEN MITIGATED (lbs)= | | | | | 67.0 | 3 | | | | |
| SITE NITROGEN LOADING RATE (lbs/ac/yr)= | | | | | 5.3 | 3 | | | | |
| TOTAL SITE NITROGEN LEFT TO MITIGATE_Wendell Only (lbs)= | | | | | 75.4 | 8 | | | | |